10 10 10 1

# STABILIZATION SYSTEM AIR TREATMENT INFORMATION PACKAGE

for the

### COMMERCIAL OIL SERVICES SITE

OREGON, OHIO

submitted to

## CITY OF TOLEDO DIVISION OF ENVIRONMENTAL SERVICES

and the

### OHIO ENVIRONMENTAL PROTECTION AGENCY

prepared by

EPA Region 5 Records Ctr. 207103

SOUND ENVIRONMENTAL SERVICES, INC.

**APRIL 16, 1997** 

# STABILIZATION SYSTEM AIR TREATMENT INFORMATION PACKAGE

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#### SECTION I INTRODUCTION

SOUND Environmental Services, Inc. (SOUND) has prepared this Stabilization System An Treatment Information Package in accordance with City of Toledo Division of Environmental Services (TDFS) and Ohio Privir amountal Protection Agency (OEPA) guidelines for the Commercial Oil Services Lagran Closure Removal Action Project in Oregon, Ohio. A site location map is shown in Figure 1.1.

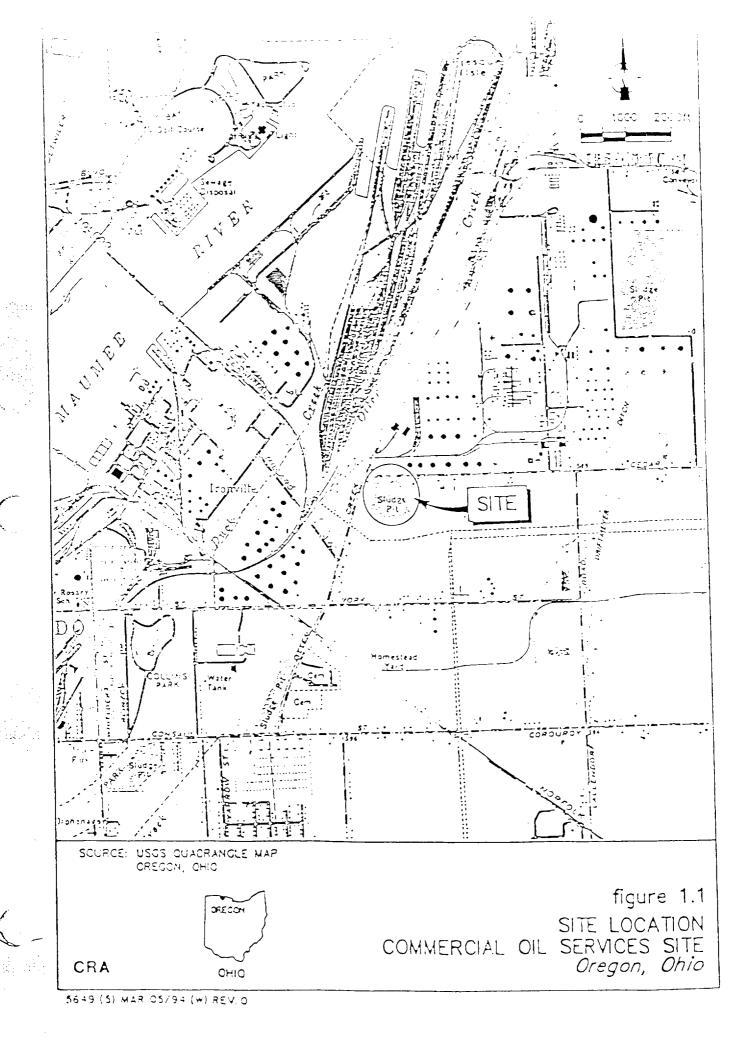
The SOUND approach to the remediation of the sludges is based upon treating pit sludges using the DCRM stabilization process and employing patented treatment equipment that incorporates emissions controls. The DCR process is a quicklime based stabilization process that, when applied to oily sludges, results in a soil-like end product. Advantages to the process are low cost, minimal volume increase, no cure period required in treatment.

This package is being submitted for TDES/OEPA review prior to mobilization and installation of the transportable treatment unit and air pollution control system which will be used to stabilize sludges on the site. This site is a Superfund Site and as thus falls under a CERCLA permit exemption from USEPA Region V. No permits are required to install and operate the stabilization system. However, the substantive requirements of the OEPA regulations must be met. This Information Package is being provided at the request of Region V to demonstrate to TEC/OEPA that the method undertaken to stabilize the sludges complies with all rules, laws, and regulations of the Ohio and US Environmental Protection Agencies.

#### Treatability Study Results

Samples provided by Conestoga-Rovers and Associates were used in developing a treatment method for this project. In the first phase of the study alternative reagents were tested to determine the most efficient method for stabilizing the sludges. In this phase, the DCR quicklime based approach was compared to using portland cement, lime kiln dust, and cement kiln dust as stabilization reagents. It was determined that the DCR process would be most effective in converting the waste sludges into a stable and solid material, and that this process would reduce overall project cost. The waste sludges were readily converted to a soil-like product using a 30% quicklime addition. The treated material could be compacted to yield a high structural strength immediately after treatment. No cure time was required





#### SECTION II TREATMENT METHOD

SOUND will implement the DCR organics stabilization process in treatment of the lagdon waste. This process offers several operational advantages over conventional cement based processes, including low volume increase and no cure period, and air pollution control.

#### Mix Design

In the treatability study performed on the samples provided, it was shown that the DCR process can be applied to the Commercial Oil sludges to produce a soil-like product. In the treatability study, both samples 24 and 30 were treated with applications of 30% calcium oxide. The resulting material is suitable for landful.

It is anticipated that the actual calcium oxide addition will vary in the field. Experience has shown that less reagent is required in full scale operations to generate an end product similar to that produced in the lab. Thus, it is our anticipation that the actual reagent application will be approximately 25%. Because there is no cure time involved in the DCR process, treatment can easily be monitored as work is ongoing. Adjustments to reagent addition can be made in real time to produce the desired end product.

One clear advantage of the DCR process is that the conversion from the liquid to the solid occurs in minutes. Literally no cure period is required. Therefore, reagent application can be varied on an ongoing basis to assure quality of treatment prior to landfill.

#### Transportable Treatment Unit Description

Reagent will be blooded with the waste in a DCR transportable treatment unit, complete with a reaction chamber and an air pollution control system (APC) to capture particulate and volatile emissions during the lime hydration reaction. This patented treatment system will consist of a self-contained mixing plant and APC equipped reaction chamber. The mixing plant, where sludges are blended with the lime reagent, consists of a feed hopper, a weigh-belt modulated feeder, a reagent holding tank and a rate modulated reagent feed system. The plant discharges into a live-floor trailer that serves as a reaction chamber where the mixture of lime and sludge react. The live floor trailer will hold the reacting waste until maximum temperatures are attained (less than 100°C).

Sludge and reagent are blended in a dual shaft pugmill mixer. Feed rates are modulated by weight. Sludge feed into the mixer is measured by a weigh-belt conveyor.

Particulates are contained and controlled through the use of a totally enclosed pneumatic reagent delivery system and reagent storage vessels equipped with particulate bag filters. The entire treatment system is enclosed to control fugitive emissions. The reagent delivery system to the mixer is equipped with closing and locking covers.

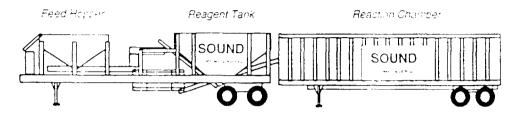
The APC withdraws vapors under negative pressure from the reaction chamber and controls volatile organic emissions from the reacting waste. The APC consists of a bag filter, catalytic oxidation unit, and caustic scrubber where the VOC's are oxidized catalytically to carbon dioxide, water vapor and inorganic acids. The caustic scrubber follows the oxidation step to neutralize the hydrochloric acid (HCl) in the air stream prior discharge to the atmosphere through a demister.

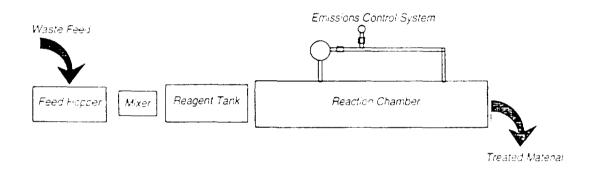


The APC is a Best Available Control Technology (BACT). Of a unit process basis in pical desirmance removal efficiencies (DEL) are as follows:

Purpose	Unit Process	Typical DRE
Particulates	Baghouse Friter	> 95%
Volatile Organics	Catalytic Oxidizer	> 95%
Acid Gas Absorption	Caustic Scrubber	> 90°;

#### Treatment Equipment Schematic





#### 24 Hour Stabilization System Performance Test

After completion of mobilization, safety training, plan approvals, and equipment shake-out activities, a 24 hour stabilization system performance test will be performed. This test will be performed while waste excavation work is being performed to consolidate lagoons 2, 3, 4, and 5 into lagoon 6. The 24 hour stabilization system performance test will be performed over three 8-hour operating days, with 3 separate stack tests being performed for the three test runs.

Use of the DCR process in waste treatment will enable shortening the duration of the 24-hour test confirmation sample period. The project specifications call for waste samples to be taken for TCLP testing at 28 days, and physical testing (unconfined compressive strength) at 1, 2, 3, 7, 14, and 28 days. However, sludge treated by the DCR process attains the majority of ultimate strength immediately after compaction. No cure period is required. Because of this characteristic, SOUND will perform both physical and chemical testing one day after treatment for each of the three test runs. The one day period reflects the average anticipated time between waste treatment, treated material stockpiling, treated material placement in the landfill and final compaction. SOUND will perform treated material testing during treatment operations at compaction. Thus, the 24 hour stabilization system performance test should be conducted to verify performance in the same time frame.

To perform the stabilization system performance test, material will be excavated from lagoon 7 and placed in a corner of lagoon 6. The sludge required for the test, approximately 1,500 yards, will be



escapated out of this location and loaded into the treatment upon. Treatest material to a visib 8-1 treatment period will be stockpiled separately for testing.

On the day following treatment, each days production will be sampled for TCLP, paint filter and compressive strength testing. The APC system stack testing will also be performed using USEPA Methods 5 and 25 as specified. Tests will be conducted on a expedited basis.

#### Interim Operation

Following completion of the stabilization system performance test, which includes submitting a summary report to the regulatory agencies complete with all analytical and physical test results which meet performance requirements, operations will be initiated on an interim basis. Interim operation will be conducted using only a single shift stabilization crew until the stabilization system performance test report is reviewed and permission is obtained to begin two shift stabilization operations. Interim operations will be initiated when the first segment of cell 1 of the landfill is ready to receive stabilization waste due to the limited space available for stockpiling stabilized material.

#### Waste Excavation, Treatment and Placement Sequencing

Waste will be loaded into the treatment unit from lagoon 6. Treated material will be discharged by a stacking conveyor. Initially the material will discharged into the first half of cell 1. This portion of the cell will be completed and separated from the rest of the cell by a temporary berm. Waste will be moved into the cell and compacted in twelve inch loose lifts. As the project progresses waste will be moved into the balance of cell 1 and compacted.

#### Air Treatment System Monitoring

Periodic checks of the stack emissions will be made throughout the project to ensure compliance with air pollution requirements. A flame ionization detector (FID) will be used to monitor inlet and outlet VOC concentrations. Dust and particulates will be monitored visually and corrective measures to control particulate discharges will be taken whenever necessary. Fugitive particulate emissions from material handling and vehicle traffic on site roads will be monitored by the site superintendent and controlled with water spray.



#### SECTION III AIR EMISSIONS ASSESSMENT / CONTROL SYSTEM DESIGN

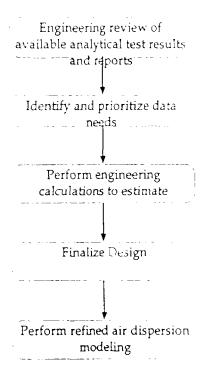
#### Introduction

This section describes the air assessment approach and presents a summary of the calculations and estimates made to determine the parameters used in the design and configuration of the air pollution control system that will be employed to control volatile organic emissions resulting from DCR stabilization / solidification of the waste sludges at the Commercial Oil Services Site in Oregan, Ohio

#### Air Emission Control Design Approach

Figure III-1 illustrates the approach used to design an optimized DCR stabilization / solidification process that the eets performance requirements.

Figure III-1 Air Emissions Control Design Approach



#### Engineering Review of Available Analytical Test Results and Reports

A review of the available reports, workplans and analytical test results from samples of waste sludges at the Commercial Oil Services Site in Oregon, Ohio, was performed to establish the basic information used in the emission control system design. The reports and information reviewed included the following:

- Treatability South, Micharen-Hart, May 8, 1992
- Phase II Removal Action Work Plan for Tank Farm and Lagoon Closure, McLaren Hort May 14, 1795
   (Revision 4)
- Revised Mass Balance Methodology, McLaren-Hart, publication date unknown
- Sampling Summary, CRA, August 22, 1996
- Sampling Results, CRA, September 23, 1996.

#### **Engineering Calculations to Estimate Emissions**

Engineering estimates were performed using experience gained during SOUND Environmental Services. Inc. stabilization /solidification project at a similar superfund site in Sand Springs, Oklahoma. At that site, a transportable treatment unit equipped with a pollution control system similar to that which will be employed at this site was used to stabilize hazardous organic sludges. The sludges contained volatile organic compounds (such as benzene) and extensive bench scale studies were performed to determine mass emission rates from the various unit processes.

The equipment utilized a live floor trailer to allow reaction of the lime waste mixture in a batch type reaction chamber. At the maximum production rate expected (75 cubic yards per hour), and the design retention time in the reaction chamber of 20 minutes, the depth of the reacting waste will be about 2 feet across the entire floor of the trailer. During the hydration reaction, this bed of reacting waste is not mixed to reduce further volatilization of organic compounds. The stabilization process is not considered a thermal desorption process. The surface area of the reacting bed is 8 feet wide by 45 feet long (360 square feet), and is the only surface area available for organics volatilization and losses.

By looking at the exposed surface area of the bed surface, it was estimated that approximately 10% of the stabilized waste would actually be exposed to induced air crossing over the reacting waste mixture. This mass, when taken at the assumed high average concentration of TCE, results in about 60 pounds per hour of total volatile organics.

#### Finalize Design

On the basis of the engineering estimates, and the air pollution system BACT requirements for the project, final design of the air pollution control system was performed. The design involved solicitation of equipment specific information from a number of vendors specializing in the manufacture of volatile organic air emissions control systems. It also involved the use of spreadsheet models for the various organic constituents, their respective vapor pressures, estimated induced air flows, estimates of available volatile organics in the stabilized waste, and design destruction removal efficiencies for the various unit processes chosen. The air pollution control system described previously in Section II was determined to be BACT for the waste stream being considered.

#### Air Dispersion Modeling

Air dispersion modeling was performed using the SCREEN3 air dispersion model recommended by the Toledo Environmental Control and Ohio EPA. Results of this modeling is presented in Section X of this package.



#### SECTION IV LOCATION / OPERATOR INFORMATION

SIINT BOYLDTHING Limbrally Mark	al Verriter Ling	Jeffary P. Bauman 9 Primary Facility Coolan		
Commercial Dil Se 2 Facility Mame	EVIDES Site	(972)		
3500 Cedar Print Road 3 Facility Address (Street)		600 East Sandy Lake Road #124. Coppell Texas [511] 11 Contact Mailing Address (Street)		
Oranon . 4 Stoy: Toesship, or Village (Sirole)		NA 12 Mail Drop/Attention (16 applicable)		
lunaa Jounty . 1 Opunty	5 Zip Code	13 City/Tawnship	Chip 14.State	
7 Obia Air Facil	ity.ID# (10-digit)	15 Zip Code	-	

8 Facility Primary Standard Industrial Code

The facility will be located on a gravel equipment pad at the northeast corner of a 5 arrecornion of the 20 acre parcel which formerly contained the tank farm area of the Commercial Dil Services Site.

16 Description of the Proposed Location of the Facility

SCINIT Environmental Services OCR Transportable Treatment Unit 17 Name of new or modified source or facility

DCR Stabilized Waste Slidge 18 Product of new or modified source/facility

Date: 4/16/97

19 Authorized Signature (for facility)

Technical Arclications Manager 20 Ditta

600 East Sandy Lake Read, #124, Coppell, Texas, 75013 21 Address (Street, City/Township State and Zip Code)

EDA FORM 3153a - 09/05

#### SECTION V EMISSIONS UNIT INFORMATION FORM

### Emissions Unit Information Form

One copy of this form should be filled out for each air pollution emissions unit covered by this information package.

25	<u>GERA Emissions Unit ID 1</u>	4. digit number):	<del></del> -	
361	Company ID for Emissions	Unit: COSS-2012-TTU-APC	:202	
27	Emilasions Vnit Activity	Description: Process Stabilization	Operation	
29		IR Stabilization Transcor	table Treatment Unit emurphi	v.:h an A.:
<u>2</u> 9.1	Construction/Modificatio	n/Emissions Testing Sche	dule DATE	
	Equipment Ordered (minth	/year'	4/37	
	Commence Construction Da	te (month/year)	5/97	
	Instial Startup Pate (mo	nth/year!	5.127	
	Most Recent Modification (as defined in OAC rule			
	<u>Performance Testing : -</u>	<del></del>	5/37	
10_	Emissions Information:			
the_e	missions unit at a rate	greater than the demi-	air pollutant proposed to be nimus amounts (list each pol	lutant on a
separ: state	ate line: and for any po or federal regulation or	Permit to Instally which	issions limit has been establi limits air emissions of the p	ollutant.
Poll	utant Name		y Emission Proposed Maxim	
Vola	tile Granica:	(1b/hr) 2	Emission (Tons/ye) 5.9	ā
· NOT	E: Volatile organics are	treated as the most pr	evalent rempound - trithlorie	thone ITCEL.
<u> </u>		is need to be identified	. copy this made and attach th	
3.	Proposed Operating Sched			
	Average Maximum	Hours Per Day 22 24	<u>Hours per Year</u> 2,400 4,600	
12.	Add-on Control Equipment Does this emissions uni If your answer is yes. In item # 34. Control Equipment Type	t employ add-on emission then fill out the table	s control equipment? 🗵 yes below. If your answer is no.	_O_ma _then_px20e20
	A. Facric filter/Baghou B. Electrostatic Precip C. Catalytic Incinerate D. Thermal Incinerator	itator E. Wet Scrubber	I. Concentrator J. Cyclone/Multiplana K. Settling Chambar L. Other describe: Oxidation/Caustin Scru	<u>Catalyti:</u> Eber
	Item Type (See Above Codes)	Control Device #1 A	Control Davide #1 Control D	Device 11
EPA F	<u>Configuration</u> ORM 1150b - 03/25	Primary	Primary	



Manufacture, a Mana

CITTARY ID

Monto, Year Installed 5/37

5.23

Pollutantisi Controlled Particulate

Volatila Craanics/Acid das

Operation Capture > 95% Efficiency %:

Avarage Dasign Control ≥ 99.53

Efficiency:3:

Operating Control NA Efficiency: 3

≥\_92₹

Inlet Gas Flow (acfr)

1.000

1.000 (maximum)

Inlet Gas Temperature (°F) 150

150

3 lb/hr

Maximum Controlled Emission NA Rate for Each Pollutant controlled (15/hr.

grain/dsof or ppmy)

Supplemental control device information (see instructions) Control Cavida #1

Comprol Device #1

Control Device #3

33. Attach a Process or Activity Flow Diagram for each emissions unit included in the application. Please see the instructions on page 17. Section VI of this package includes a process flow diagram for the emissions unit.

Emissions edress point(s) information: (Provide the following information for each point at which emissions are released into the ambi: 1 air from the emissions unit. List each individual egress point on a separate linel:

Egress coint type codes:

A. vertical stack (unobstructed) C. vertical stack (obstructed) B. horizontal(downward stack D. fugitive B. horizontal/downward stack

Egresa Point

Information Company ID for Egrass Point		Egress Point Share (ff)	Egress Height Ifth	Temp (F)	Flow (ACFM.	GER Building Height /fl:	GER Building Length (ft.
Stack 031	A	0.5	20	150	1000	29	<u> 25</u>

EMISSIONS UNIT EGRESS POINT

LOCATION INFORMATION

Company ID UTM Zone
for Exress [16 or 17]

UTM Easting UTM Northing Base Elevation Minimum 15 digit) (m) 17 digit) (m) 1ft) Eencelis

<u>Fenceline</u> Pistance (ft)

Paint Stack COL

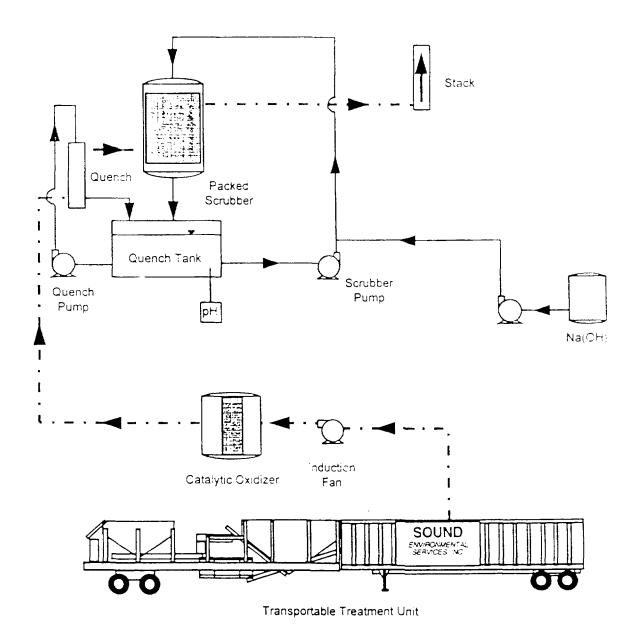
ERA FORM 31535 - 28/35

Ask you applying, per CAC rule 1745-25-25, for fiderally enforceable in the as pain in ti. : pertit :: vance? 🗆 yes 🧸 no

- Are windresting any information included in this application for this emissions unit is 36.
- Pres into emissions unit utilize any continuous emissions monitoring emismant) if accomplete the following table. The monitoring will be periodically menitored manually.

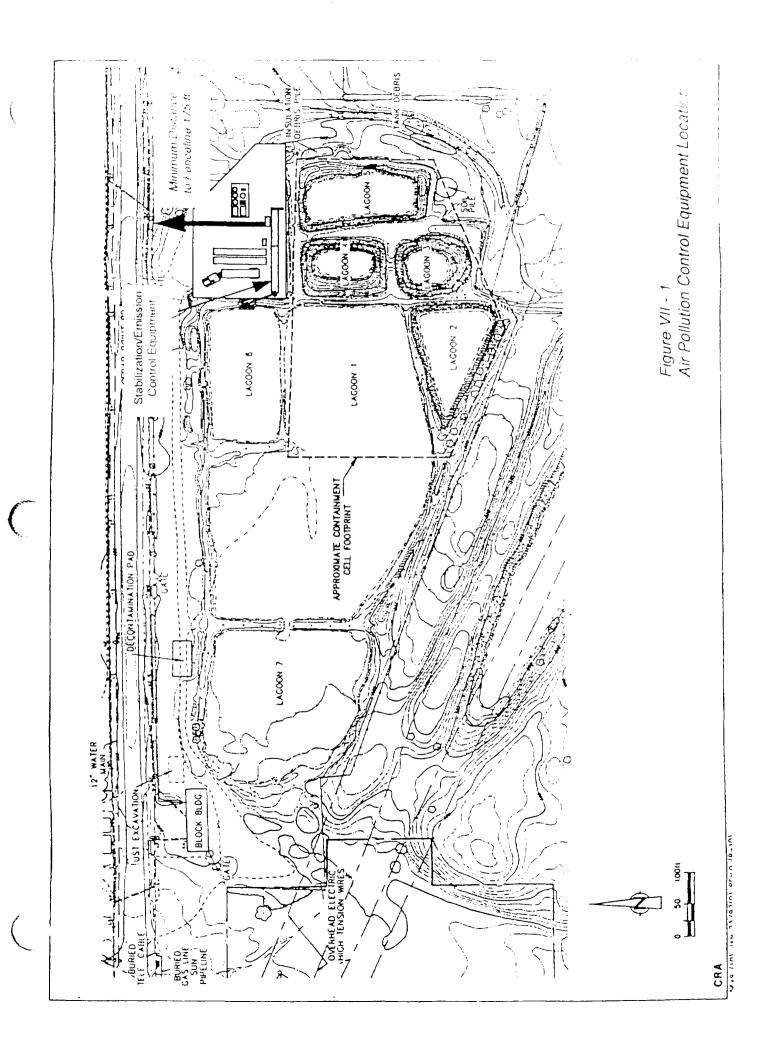
Company ID for Type of Monitor Manufacturer: Serial Number Poliutantial Model Number Monitored

The appropriate Emissions Activity Category (FAC) formis) must be completed and attached for each emissions unit. At least one complete FAC form must be submitted for each emission unit for the application to be considered compete. 39.



SECTION VII EQUIPMENT LOCATION DRAWINGS

SOUND ENVIRONMENTAL SERVICES, INC.



## EMISSIONS ACTIVITY CATEGORY FORM PROCESS OPERATION

	OEPA EMISSIONS U	NIT ID	(if establishe	d)		
	e: If there is more than one tional product (see instruc		cess, copy and complete this	page for each		
1.	End product of this proc	ess: <u>DCR Stabi</u>	lized Sludge			
2.	Hourly production rates (indicate appropriate units):					
	Average production: Maximum production:	50 tons/h 75 tons/h	50 tons/hour 75 tons/hour			
3.	Projected maximum annual production (indicate appropriate units): 100,000 tons					
4.	Actual annual production (indicate appropriate units): NA					
5.	Type of operation: Hazardous waste stabilization / solidification					
6.	Materials used in proce	ss at maximum hourly p	roduction rate:			
	Material	Physical State at Standard Conditions	Principle Use	Amount (lbs/hr)		
Qu	icklime	Solid	Stabilization Reagent	45,000		
Wa	ater	Liquid	Wetting Agent, hydration	15,000		
-						

REV 1995 1 of 1



#### SECTION IX ADDITIONAL INFORMATION FORM

#### Additional Information Form

EFA FORM 3150s - 08/95

The following additional information is being submitted with the information parkage. This additional information is divided into four sections: General information which is required information required for air pollution applications, information required for wastewater applications and information required for solid waste disposal facilities.

Additio	onal Information			
1.	Will the proposed source/fs	cility involve any o	of the following (Check all that	Apply(?
	⊠ Air Discharge  ☐ Wastewater Treatment Wor		Solid Waste Disposal Facility Kazardous Waste Disposal Facilit	у
2 .		reconstruction of an	is a new installation, modific existing source/facility, or a down for <u>year?</u>	
	This is a new installate exemption.	on of a temporary	system under a superfund Ca	SECTA DESTRICT
3_	source/facility? If so, st	ate the date and ty	plan submission been file ge of application previously sub DAir D Solid Waste Wastewater D Harardous Was	ritted.
4	Will the proposed source/fo	agility comply with 1_nc	all rules, laws, and repulations	of Ohio EPA
5	Do you wish to request per 3745-31-25(E)? 🗆 yes	mit to install regis	itration status via Ohio Adminis	mrative 2:d=
<u>5.</u>	Are the proposed sources Note: Don't be afraid to emissions units need to por	call your Ohio EPA	with the following federal : field office contact to ask dards.	them if your
	_O_yes 8_no New	Source Performance S	tandards (NSPS)	
	nary Sources. If your em:		CFR 60 - Standards of Perform listed under one of these st	
	□ yas ⊠ no Nati	onal Emission Stand	urds for Hagardous Air Pollutant	a MESHARS.
	al Emissions Standards for ons unit(s) are listed under		tants are listed under 40 CFR urds then answer yes.	<pre>\$1. If your</pre>
	_D_yes8_no Maxx	mum Available Contr	ol Technology (MACT) Standards	
	ximum Available Control Tech s) are listed under on of th		e listed under 40 CFR 63. If y answer yes.	our emissions
	_O_yes S_no Prev	ention of Significa	nt Deterioration (PSD)	
These	rules are found under 40 CF1	8 51.21,		
	_O_yesS no Apps	endix 'S' - Emission	Offset Policy	
This p		Appendix S to 40 C	FR part 51 - Emissions Offset	Interperativo
remit			ble? (i.e. 40 CFR Part 3	'5 Title IV



<b>.</b>	Will the product months units excity best available two-multon .EAT. 1. This is
	required under this Asymptotive Code 1745-31-15 April . The definition of bust
	available termology can be found in Chio Revised Tode 3704.1117 and is defined as:
	Best Available Control Technology' means an emissions limitation (including a visible
	emissions standard; based upon the maximum degree of reduction for each pollutant subject
	to regulation under the clean air act which would be emitted from any proceed major
	stationary source or major medification which the director on a case-by-case basis.
	taking into account energy, environmental and economic impacts and other dosts, determines
	is agrievable for such major stationary source or major modification through application
	of production processes or available methods, systems and techniques, including fuel
	combustion techniques for control of such pollutant.

<u>aey\_</u> \_\_\_\_

8. Will the proposed emissions unity facility comply with all rules, lews, and regulations of the Chic EPA and U.S. EPA2

N\_Yes\_\_\_O\_n:

9. Will the proposed sources cause the significant degradation of air quality?

D\_Yaz \_\_\_B\_nq

1). Will the proposed sources interfere with the attainment and maintenance of the ambient air quality standards?

□<u>ves</u> ⊠<u>no</u>

11. Describe any emissions unit monitoring, emission monitoring, or dentrol equipment monitoring devices to be installed by the applicant which are not already described in the attached Brissions Activity Form(s).

Emissions unit monitoring will be performed using a flame Ionization detector calibrated for the compounds of concern after the initial startup system performance stack testing using EPA methods 5 and 25.

Will the proposed emissions unit(s) involve the use of astestos, benzene, beryllium, mentury, or vinyl chloride?

□ yes ⊠ no Asbestos

□ yes ⊠ no Benzene

□ <u>ves ⊠ no Renyllium</u>

□ yes 🗵 co Vinyl Chloride

II. Please include the estimated rost of any air pollution control equipment to be installed on the processed emissions unit(s).

The estimated cost of the air pollution control equipment including the reaction sharber, catalytic exidation unit, and caustic scrubber unit is \$200,000.00

EPA FORM 3150d - 08/35

SOUND ENVIRONMENTAL SERVICES, INC

04/15/97 09:50:36

\*\*\* SCREEN3 MODEL RUN \*\*\*

\*\*\* VERSION DATED 95250 \*\*\*

COMMERCIAL OIL SERVICES SITE

SIMPLE TERRAIN INPUTS.

SOURCE TYPE = POINT

EMISSION RATE (G/S) = .328000

STACK HEIGHT (M) = 6.5600

STK INSIDE DIAM (M) = .1640

STK EXIT VELOCITY (M/S)= 24.5759

STK GAS EXIT TEMP (K) = 338.0000

AMBIENT AIR TEMP (K) = 293.0000

RECEPTOR HEIGHT (M) = 2.0000

URBAN/RURAL OPTION = RURAL

BUILDING HEIGHT (M) = .0000

MIN HORIZ BLDG DIM (M) = .0000

MAX HORIZ BLDG DIM (M) = .0000

STACK EXIT VELOCITY WAS CALCULATED FROM VOLUME FLOW RATE = 1100.0000 (ACFM)

BUOY. FLUX = .216 M\*\*4/S\*\*3; MOM. FLUX = 3.520 M\*\*4/S\*\*2.

\*\*\* FULL METEOROLOGY \*\*\*

\*\*\* SCREEN ALTOMATED DISTANCES \*\*\*

\*\*\* SCREEN AUTOMATED DISTANCES \*\*\*

\*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\*

DIST CONC U10M USTK MIX HT PLUME SIGMA SIGMA (M) (UG/M\*\*3) STAB (M/S) (M/S) (M) HT (M) Y (M) Z (M) DWASH

1. .0000 1 1.0 1.0 320.0 18.65 1.28 1.22 NO

100. 147.8 3 2.5 2.5 800.0 11.40 12.54 7.57 NO

200. 137.5 4 2.0 2.0 640.0 12.61 15.66 8.67 NO

MAXIMUM 1-HR CONCENTRATION AT OR BEYOND 1. M: 100. 147.8 3 2.5 2.5 800.0 11.40 12.54 7.57 NO

DWASH= MEANS NO CALC MADE (CONC = 0.0)

DWASH=NO MEANS NO BUILDING DOWNWASH USED

DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED

DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED

DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB



\*\*\* SCREEN DISCRETE DISTANCES \*\*\* \*\*\* TERRAIN HEIGHT OF 0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES \*\*\* DIST CONC U10M USTK MIX HT PLUME SIGMA SIGMA (M)  $(UG/M^{**3})$  STAB (M/S) (M/S) (M) HT (M) Y (M) Z (M) DWASH ------57. 128.7 2 3.0 3.0 960.0 10.59 11.59 6.38 NO DWASH= MEANS NO CALC MADE (CONC = 0.0) DWASH=NO MEANS NO BUILDING DOWNWASH USED DWASH=HS MEANS HUBER-SNYDER DOWNWASH USED DWASH=SS MEANS SCHULMAN-SCIRE DOWNWASH USED DWASH=NA MEANS DOWNWASH NOT APPLICABLE, X<3\*LB \*\*\*\*\*\*\*\*\*\*\* \*\*\* SUMMARY OF SCREEN MODEL RESULTS \*\*\* CALCULATION MAX CONC DIST TO TERRAIN PROCEDURE (UG/M\*\*3) MAX (M) HT (M) SIMPLE TERRAIN 147.8 100. 0. \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* \*\* REMEMBER TO INCLUDE BACKGROUND CONCENTRATIONS \*\*

## COMMERCIAL OIL SERVICES SITE, OREGON, OHIO AIR DISPERSION MODELING SUMMARY SHEET

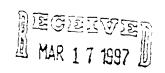
POIN	I SOURCE S	CKEEN3 I	ABLE (METRIC)			
TEMP out	338	K	BUILDING	NO	FLOWacfm [1]	1100
TEMP amb	293	K	U/RURAL	RURAL	:	. 0
EMISS rate	148.8	g/s	RECEPTOR	2.0 m		

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> 72 42 = 4476 Tolvere



# UNITED STATES ENVIRONMENTAL PROTECTION AGENCY REGION 5 77 WEST JACKSON EQULEYARD CHICAGO, IL 60604-3590



REPLY TO THE ATTENTION OF

SR-6J

March 11, 1997

James Campbell, Ph.D., P.E. Engineering Management, Inc. 2020 Ardmore Boulevard Suite 327 Pittsburgh, PA 15291 Aloysius Aguwa, Ph.D. Altech Environmental Services 24175 Northwestern Highway Suite 3 Southfield, MI 48075

#### VIA TELEFAX AND FIRST CLASS U.S. MAIL

Re: Draft Risk-Based Remediation Goals Assessment (RGA) and Remedial Action (RA) Design Documents for the Lagoon Closure Removal Action, Commercial Oil Services Site, Oregon, Ohio

Dear Drs. Campbell and Aguwa:

The U.S. EPA and its consultant, Ecology and Environment, Inc., have reviewed the draft RGA document of February 24, 1997 and the RA Design and Construction Documents (volumes 1-3 and drawings) of February 20, 1997 for the Lagoon Closure Removal Action at the Commercial Oil Services (COS) site. These documents are required as per the Phase II Administrative Order by Consent, effective February 17, 1994. This most recent draft was resubmitted to the Agency in response to our letter of February 19, 1997 in which U.S.EPA required additional modifications to the documents in order to meet with its approval.

U.S.EPA finds that the requested changes have been made to the RGA and RA Design Documents in accordance with its specifications and that the Final Design meets the Comprehensive Environmental Response, Compensation and Liability Act (CERCLA) requirements. The COS Phase II Group respondents are hereby notified that these documents are approved by U.S. EPA.

The Agency is in the process of completing the edministrative procedures necessary to secure removal action oversight support for this project under the new regional contract, and will keep

you apprised of the situation. In the mean time, if you have any questions regarding the contents of this letter, please do not hesitate to contact me at (312) 886-5251.

Sincerely,

Sheila A. Sullivan

Removal Project Manager

U.S. EPA, Region V

cc: E. Peterson, COS Technical Committee

- A. Van Norman, CRA
- T. Huntrods, CRA
- D. Haynam, Fuller & Henry
- B. Horenziak, E & E
- D. Tiebout, E & E
- R. Murawski, U.S. EPA, ORC
- D. Ballotti, USEPA
- B. Sypniewski, USEPA, RRB

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